

Probabilistic characteristics of narrow-band long wave run-up onshore by Sergey Gurbatov and Efim Pelinovsky

First of all, we would like to thank two anonymous reviewers for their useful comments and suggestions. An item-by-item response on all the comments is presented below.

Referee #1

The NHESS paper 2019-176 “Probabilistic characteristics of narrow-band long wave run-up onshore” by Gurbatov and Pelinovsky presents an interesting analysis of random, long-wave runup with amplitudes and phases of offshore waves defined probabilistically. The paper is well organized and, except for some minor clarifications listed below, is well written. Important conclusions are given with regard to the validity of linear theory for runup and inundation probability distributions. Given the scope of the journal, it would be advisable to indicate how the results from this study impact current probabilistic long-wave hazard assessments, as indicated in Comment 1. Overall, the nature of the comments below, in my opinion, are minor. Upon revision, this paper should be an important contribution to NHESS.

Technical comments:

(1) For probabilistic tsunami hazard assessments (PTHAs) in particular, there have been several recent studies that approximate runup and inundation from a probabilistic determination of offshore wave characteristics as summarized by Grezio et al. (2017). For example, Lorito et al. (2015) use a Green’s Law approximation to estimate inundation. Davies et al. (2017) use an “amp-factor” method derived from Løvholt et al. (2012). Similarly, Mueller et al. (2015) use “linear predictors” to estimate runup. Can the results of the authors’ study be used to evaluate these various PTHA runup/inundation estimators?

Actually, it is a very important discussion connected with the applicability of various runup formulas. Some of them (for example, Green’s Law) are particular cases of analytical formulas used in our approach. In fact, they are used to analyze the tsunami waves which are not a stationary random process. The study of such processes is beyond scope of our paper where we try to get analytical results in the case of input signals presented as the stationary random processes (swell, seiches, the atmospheric origin tsunami etc). We would not discuss in our paper this important discussion suggested by the reviewer.

(2) L36: Løvholt et al. (2012) indicate that the hydrostatic assumption reduces runup variability, compared to including dispersion.

It is an important comment, therefore, we added the final paragraph in conclusion: **Now in practice various generalizations of shallow-water equations are used to analyse the tsunami runup including wave dispersion, see, for instance (Løvholt et al, 2012). Wave dispersion as a quadratic dissipative term prevents us from getting analytical results, so their influence on statistical characteristics should be investigated in future.**

(3) L46-56: *Should also probably summarize the work of Carrier (1995) and Carrier et al. (2003).*

These papers are included in the list of references.

(4) L111-112: *It is worth noting that Carrier (1995) also derives runup from along-shore (i.e., edge wave) propagation.*

Yes, we know these results were also published in the JFM paper as well as the results given by Brocchini. However, these results are approximated and not quite good for the rigorous theory.

(5) Eqns. 2.5-2.8: *Carrier (1995) includes quadratic terms in these equations, deemed negligible.*

The quadratic dissipative term is widely used in practice, but in the rigorous benchmark theory there are no analytical results, and the analysis of such equations are beyond scope of this paper.

(6) *It might not be advisable to include Section 6, since as the authors indicate, the complex interaction of breaking waves is not included.*

We absolutely agree with this comment. That is why our text after Fig. 9 contains the following conclusion: “This important issue requires going beyond the theory discussed in this article”. We slightly modified the final paragraph going after Fig. 9 by saying:

However, these results should be treated with caution. **If $Br > 1$ the Jacobian breaks down seawards of the shoreline. This may affect the probabilistic distribution on the positive side.** This important issue requires going beyond the theory discussed in this article

Grammatical/typographical comments:

(7) Citation formatting: when the authors are part of the sentence, do not place in parentheses (L46, 64, 171-173, 186).

Done

(8) L29-31: *Important first sentence is awkwardly constructed.*

The sentence has been modified and runs as follows: The flooded area size, the water flow depth and its speed on the coast, the coastal topography characteristics determine the consequences of marine natural disasters on the coast

(9) L44: *Space between “linearized” and “by”.*

Done

(10) L58-59: *“Moreover, very often the leading wave turns out <not> to be the maximum one.”*

The sentence is modified: Moreover, very often the leading wave **is not** the maximum one.

(11) L62: *“their help” is confusing.*

Deleted

(12) L80 and elsewhere: Most likely “simple” wave equation will be misunderstood by most readers as an alternative name for the Riemann wave equation.

Unfortunately, the term “the simple wave equation” is used more often than “the Riemann wave equation”. It is why we would like to use both terms.

(13) L99: “climbs”->”approaches”

Done

(14) L169: Which equation does “ODE” refer to?

Corrected, the following items have been inserted: Eqs. (2.11) and (2.12)

(15) L182: Remove hyphen before *Br* (could be interpreted as a negative sign)

Done

(16) L184: What does “last sea particle acceleration” mean?

The last sea particle acceleration ($\alpha^{-1}d^2R/dt^2$) means the acceleration of **the** moving shoreline along the slope in **the** linear theory.

(17) L224-225: Awkward sentence.

The sentence “Formula (3.6) allows working further with the run-up height R_0 instead of the wave amplitude far from the coast $a(x)$, considering it to be given” replaced by:
Formula (3.6) allows working further with the run-up height R_0 instead of the wave amplitude far from the coast $a(x)$. **This run-up height will be considered as the given value.**

(18) L238: “what is another record” -> “which is another expression”

Done

(19) Fig. 2 caption: Indicate that this is for monochromatic waves?

Added: **in the case of the incident monochromatic wave**

(20) L266-267: insert “ W ” after “vertical displacement” (correct?) How is W related to R , as a random variate?

Thank you for the comment, Eq. (4.1) is now re-written in the dimensionless form, and all the values are understood. In fact, $W(z)dz=W(r)dr$, and, therefore, $W(r)=W(z=r/R_0)/R_0$

(21) L274: Replace Russian character for “and” with English equivalent.

Done

(22) L308: “the equation mentioned last” -> “the last equation”

Changed into equation (3.12)

(23) L351: Indicate that the Rayleigh distribution is for wave heights.

Corrected. It is now given in L353.

References:

Carrier, G.F., 1995. On-shelf tsunami generation and coastal propagation. in *Tsunami: Progress in Prediction, Disaster Prevention and Warning*, pp. 1-20, eds. Tsuchiya, Y. & Shuto, N. Kluwer, Dordrecht, The Netherlands.

Carrier, G.F., Wu, T.T. & Yeh, H., 2003. Tsunami run-up and draw-down on a plane beach, *Journal of Fluid Mechanics*, 475, 79-99.

Davies, G., Griffin, J., Løvholt, F., Glimsdal, S., Harbitz, C., Thio, H.K., Lorito, S., Basili, R., Selva, J., Geist, E.L. & Baptista, M.A., 2017. A global probabilistic tsunami hazard assessment from earthquake sources. in *Tsunamis: Geology, Hazards and Risks*, pp. doi:10.1144/SP1456.1146, eds. Scourse, E. M., Chapman, N. A., Tappin, D. R. & Wallis, S. R. Geological Society of London Spec. Pub. 456, London.

Grezio, A., Babeyko, A.Y., Baptista, A.M., Behrens, J., Costa, A., Davies, G., Geist, E.L., Glimsdal, S., González, F.I., Griffin, J., Harbitz, C.B., LeVeque, R.J., Lorito, S., Løvholt, F., Omira, R., Mueller, C.S., Paris, R., Parsons, T., Polet, J., Power, W., Selva, J., Sørensen, M.B. & Thio, H.K., 2017. Probabilistic Tsunami Hazard Analysis (PTHA): Multiple sources and global applications, *Reviews of Geophysics*, 55, 1158-1198.

Lorito, S., Selva, J., Basili, R., Romano, F., Tiberti, M.M. & Piatanesi, A., 2015. Probabilistic hazard for seismically induced tsunamis: accuracy and feasibility of inundation maps, *Geophys. J. Int.*, 200, 574-588.

Løvholt, F., Pedersen, G., Bazin, S., Kühn, D., Bredesen, R.E. & Harbitz, C., 2012. Stochastic analysis of tsunami runup due to heterogeneous coseismic slip and dispersion, *J. Geophys. Res.*, 117, doi: 10.1029/2011JC007616.

Mueller, C., Power, W., Fraser, S. & Wang, X., 2015. Effects of rupture complexity on local tsunami inundation: Implications for probabilistic tsunami hazard assessment by example, *Journal of Geophysical Research: Solid Earth*, 120, 488-502.

Referee #2

The paper presents a theoretical study of random long wave run-up over a plane beach. It starts with a general introduction of the well-known Carrier-Greenspan approach and then describes linear and nonlinear shoreline dynamics of monochromatic waves. The early sections provide reviews of previous works by the authors. The novelty of this work lies in the probabilistic analysis of shoreline displacement and velocity in the latter sections. The authors apply the geometric probability theory for shoreline dynamics to compare statistical properties of linear and nonlinear wave run-up on the shore. Although the approach has significant limitations (e.g. non-breaking and nondispersive long waves), the paper provides a statistical view of nonlinear wave runup which is of interest to the community. I recommend publication of the paper after following comments are addressed.

-There are typos, missing spaces between words and grammatical errors. Please edit the paper carefully.

Corrected

-The equation (4.1) is a bit confusing. The RHS of the equation appears to have dimension after reading from the previous sections. Please improve the notation for readers who are not very familiar with the geometric probability theory.

Thank you for the comment. We have re-written equation (4.1) in dimensionless variables. This comment is also used to modify Fig. 2 in the dimensionless form.

-The assumption of “narrow band” is not clearly explained. In section 5, the incident wave is introduced as “a quasi-harmonic wave with a random amplitude and phase” (L328). The authors do not mention anything about wave period.

We have added the definition of the narrow-band wave field (see answer on next comments):
The narrow-band random wave field contains sine waves with almost constant frequency and random amplitude and phase.

-L340-349: Is it obvious that narrow-band random waves exhibit non-breaking wave run-up if individual monochromatic waves are below the breaking criterion? This seems to require certain assumptions or some explanation at least.

We slightly modified the text in lines L340-349:

Formula (5.4) has an important practical meaning: by the measured distribution of the wave amplitudes far from the coast (re-computed on run-up amplitudes in the linear theory), it is possible to obtain the distribution of the wave run-up characteristics on the coast. The only requirement imposed on the wave ensemble is that it should not contain breaking waves, which should be somehow removed from the record. It immediately follows that the Gaussian field containing large amplitude tails does not fit this requirement, and it should be modified. Therefore, we assume the amplitude distribution to be finite for $A < A_{max} = 1$. **The narrow-band random wave field contains sine waves with almost constant frequency and random amplitude and phase. It means that if the wave amplitude is below the “breaking amplitude” $A_{max} = 1$, the breaking will not be implemented in any way, and the random wave run-up will take place without any breaking.** Further calculations depend on the specific type of the amplitude distribution.

-The result of broken wave runoff in Section 6 may be questionable. The setting with $Br=2$ implies that wave breaking occurs before the incident waves arrive at the shore (The Jacobian breaks down seawards of the shoreline). This may affect the probabilistic distribution by eliminating the tail on the positive side.

We absolutely agree with this comment. That is why our text after Fig. 9 contains the following conclusion: “This important issue requires going beyond the theory discussed in this article”. We slightly modified the final paragraph that goes after Fig. 9 by saying:
However, these results should be treated with caution. **If $Br > 1$ the Jacobian breaks down seawards of the shoreline. This may affect the probabilistic distribution on the positive side.** This important issue requires going beyond the theory discussed in this article

Probabilistic characteristics of narrow-band long wave run-up onshore

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Abstract

The run-up of random long wave ensemble (swell, storm surge and tsunami) on the constant-slope beach is studied in the framework of the nonlinear shallow-water theory in the approximation of non-breaking waves. If the incident wave approaches the shore from deepest water, runup characteristics can be found in two stages: at the first stage, linear equations are solved and the wave characteristics at the fixed (undisturbed) shoreline are found, and, at the second stage, the nonlinear dynamics of the moving shoreline is studied by means of the Riemann (nonlinear) transformation of linear solutions. In the paper, detail results are obtained for quasi-harmonic (narrow-band) waves with random amplitude and phase. It is shown that the probabilistic characteristics of the runup extremes can be found from the linear theory, while the same ones of the moving shoreline - from the nonlinear theory. The role of wave breaking due to large-amplitude outliers is discussed, so that it becomes necessary to consider wave ensembles with non-Gaussian statistics within the framework of the analytical theory of non-breaking waves. The basic formulas for calculating the probabilistic characteristics of the moving shoreline and its velocity through the incident wave characteristics are given. They can be used for estimates of the flooding zone characteristics in marine natural hazards.

Keywords: tsunami, storm surge, long wave runup, Carrier-Greenspan transform, statistical characteristics

1. Introduction

The flooded area size, the water flow depth and its speed on the coast, the coastal topography characteristics ~~and the features of the coastal zone development~~ determine the consequences of marine natural disasters on the coast. The catastrophic events of recent years are well known, when tsunami waves and storm surges caused significant damage on the coast and people's death. It is worth saying that only in 2018 two catastrophic tsunamis occurred in Indonesia, leading to the death of several thousand people (on Sulawesi Island in September and in the Sunda Strait in December). The calculations of the coast flooding due to tsunamis and storm surges are mainly carried out within the framework of nonlinear shallow-water equations, taking into account the variable roughness coefficient for various areas of the coastal zone (Kaiser et al,

38 2011; Choi et al, 2012). The characteristics of the coastal destruction is determined either by
39 using fragility curves (Macabuag et al, 2016; Park et al, 2017) or by using a direct calculation of
40 the tsunami forces (Qi et al, 2014; Ozer et al, 2015a, b; Kian et al, 2016; Xiong et al., 2019).

41 The computation accuracy was tested on a series of benchmarks, including the idealized
42 problem of the wave run-up onto the impenetrable slope of a constant gradient without friction
43 (Synolakis et al, 2008). The nonlinear shallow water equations for the bottom geometry of this
44 kind are linearized by using the hodograph (Legendre) transformations. This step makes it
45 possible to obtain a number of exact solutions describing the run-up on the coast. This approach,
46 first suggested by Carrier and Greenspan (1958), was later on used to analyze the run-up of
47 single and periodic waves of various shapes (Synolakis, 1987; Pelinovsky and Mazova, 1992;
48 Carrier, 1995; Carrier et al, 2003; Tinti and Toniti, 2005; Madsen and Fuhrman, 2008; Madsen
49 and Schaffer, 2010; Antuano and Brocchini, 2008, 2010; Didenkulova, 2009; Dobrokhotov et al,
50 2015; Aydin and Kanoglu, 2017). Moreover, such approach made it possible to determine the
51 conditions for the wave breaking. The latter means the presence of steep fronts (gradient
52 catastrophe) within the hyperbolic shallow water equation framework. The Carrier-Greenspan
53 transformation was further generalized for the case of waves in an inclined channel of an
54 arbitrary variable cross section (Rybkin et al, 2013; Pedersen, 2016; Shimozone, 2016; Anderson
55 et al, 2017; Raz et al, 2018). In a number of practical cases, its use proves to be more efficient
56 than the direct numerical computation within the 2D shallow water equation framework (Harris
57 et al, 2015, 2016).

58 Due to bathymetry variability and shoreline complexity, diffraction and scattering effects
59 lead to an irregular shape of the waves approaching the coast. Moreover, very often ~~not~~ the
60 leading wave ~~is not turns-out-to-be~~ the maximum one. Such typical tsunami wave records on
61 tide-gauges are well known and are not shown here. It is applied even more to swell waves,
62 which in some cases approach the coast without breaking (Huntley et al, 1977; Hughes et al,
63 2010). As a result, statistical wave theory can be applied to such records and ~~with their help,~~
64 nonlinear shallow water equations in the random function class can be solved. This approach was
65 used to describe the statistical moments of the long wave run-up characteristics in (Didenkulova
66 et al, 2008, 2010, 2011). Special laboratory experiments were also conducted on irregular wave
67 run-up on a flat slope, the results of which are not very well described by theoretical
68 dependencies (Denissenko et al, 2011, 2013). As for field data, we are acquainted with two
69 papers: (Huntley et al, 1977; Hughes et al, 2010), where the statistical characteristics of the
70 moving shoreline on two Canadian and one Australian beaches were calculated. They confirmed
71 the fact that the wave process on the coast is not Gaussian. In our opinion, the main problem in

72 the theoretical model of describing the irregular wave run-up on the shore is associated with the
73 use of two hypotheses: 1) the small amplitude wave field (in the linear problem) is Gaussian; 2)
74 waves run-up on the shore without breaking. It is obvious, however, that in the nonlinear wave
75 field some broken waves can always be present. They affect the distribution function tails and,
76 thus, the statistical moments of the run-up characteristics as well.

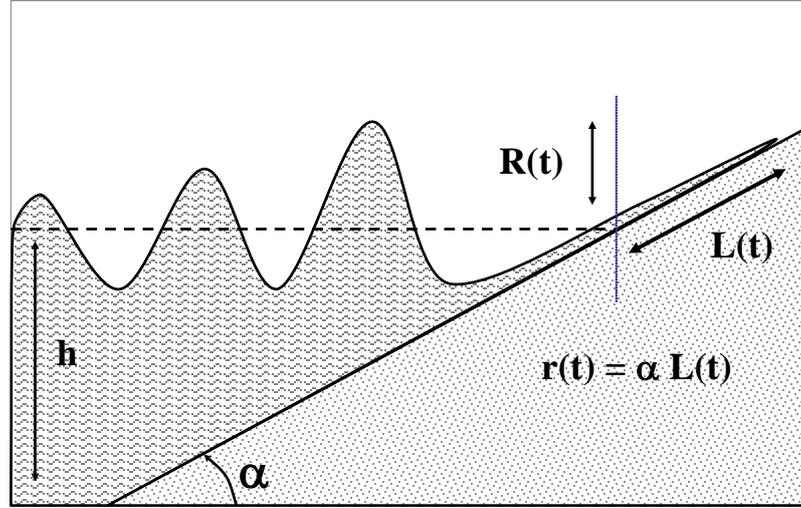
77 The connection of the run-up parameters at the nonlinear stage with the linear field at a
78 fixed point is described either in a parametric form or implicitly in a nonlinear equation
79 (Didenkulova et al., 2010). This does not allow using the standard methods of random processes.
80 At the same time, it is known, that this implicit equation is equivalent to a partial first-order
81 differential equation (PDE), that is, to the simple (the Riemann wave) equation (Rudenko and
82 Soluyan, 1977). In statistical problems, this equation arises in nonlinear acoustics. This equation
83 or its generalization, the nonlinear diffusion equation called the Burgers equation (Burgers et al,
84 1974) is the model equation in the hydrodynamic turbulence theory (Frisch, 1995). It should be
85 noted that for the one-dimensional Burgers turbulence, as well as its three-dimensional version,
86 used for the model description of the large-scale Universe structure (Gurbatov et al, 2012). It is
87 possible to give an almost comprehensive statistical description for certain initial conditions
88 (Gurbatov et al, 1991, 1997, 2011; Gurbatov and Saichev, 1993; Molchanov et al, 1995; Frisch,
89 1995; Woyczynski, 1998; Frisch and Bec, 2001; Bec and Khanin, 2007). In particular, single-
90 point and two-point probability distributions of the velocity field and even N -point probability
91 distributions and, accordingly, multi-point moment functions were found. This partially allows
92 using a mathematical approach developed in statistical nonlinear acoustics. An experimental
93 study of the nonlinear evolution of random quasi-monochromatic waves and the probability
94 distributions and spectra analysis have been carried out in acoustics more than once. They
95 confirmed theoretical conclusions; see, for example (Gurbatov et al, 2018, 2019).

96 This paper is devoted to the analytical study of the probabilistic characteristics of the long
97 narrow-band wave run-up on the coast. Section 2 gives the basic equations of nonlinear shallow
98 water theory and the Carrier-Greenspan transformation, with the latter making it possible to
99 linearize the nonlinear equations. Section 3 describes the moving shoreline dynamics when the
100 deterministic sine wave ~~approaches~~ ~~climbs~~ the slope. The probability characteristics of the
101 deformed sine oscillations of the moving shoreline with a random phase are described in Section
102 4. Section 5 contains the probabilistic characteristics on the vertical displacement of the moving
103 shoreline if the incident narrow-band wave has a random amplitude and phase. The discussion of
104 the wave breaking effects and their influence on the distribution of the run-up characteristics is
105 given in Section 6. The results obtained are summarized in Section 7.

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2. Basic equations and transformations



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Fig. 1. The problem geometry

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Here we will consider the classical formulation of the problem of a long wave run-up on the constant-gradient slope in an ideal fluid (Fig. 1). The wave is one-dimensional and propagates along the x -axis directed onshore. The basin depth is a linear depth function: $h(x) = -\alpha x$, where α is the inclination angle tangent and point $x = 0$ corresponds to a fixed unperturbed water shoreline. $L(t)$ and $r(t)$ describe the horizontal and vertical displacement of the moving shoreline, and $R(t)$ is the water level oscillations at $x = 0$. The bottom and the shore are assumed impenetrable. The long wave dynamics is described by nonlinear shallow water equations:

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$$\frac{\partial u}{\partial t} + u \frac{\partial u}{\partial x} + g \frac{\partial \eta}{\partial x} = 0, \quad (2.1)$$

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$$\frac{\partial \eta}{\partial t} + \frac{\partial}{\partial x} [(-\alpha x + \eta)u] = 0. \quad (2.2)$$

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121

122

Here, $\eta(x,t)$ is the free surface elevation above the undisturbed water level, and $u(x,t)$ is the depth-averaged flow velocity (within the shallow water theory, the flow velocity is the same on all horizons), and g is the gravity acceleration. Obviously, after introducing total depth

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$$H(x,t) = -\alpha x + \eta(x,t), \quad (2.3)$$

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equations (2.1) and (2.2) are a hyperbolic system with constant coefficients. This fact makes it possible to transform the system into a linear equation one by using a hodograph (Legendre)

126 transformation, which was done in the pioneering work (Carrier and Greenspan, 1958). As a
 127 result, the wave field is described by a linear wave equation in the ‘cylindrical’ coordinate
 128 system

$$129 \quad \frac{\partial^2 \Phi}{\partial \lambda^2} - \frac{\partial^2 \Phi}{\partial \sigma^2} - \frac{1}{\sigma} \frac{\partial \Phi}{\partial \sigma} = 0, \quad (2.4)$$

130 and all variables are expressed in terms of an auxiliary wave function $\Phi(\sigma, \lambda)$ using explicit
 131 formulas

$$132 \quad \eta = \frac{1}{2g} \left(\frac{\partial \Phi}{\partial \lambda} - u^2 \right), \quad (2.5)$$

$$133 \quad u = \frac{1}{\sigma} \frac{\partial \Phi}{\partial \sigma}, \quad (2.6)$$

$$134 \quad x = \frac{1}{2\alpha g} \left(\frac{\partial \Phi}{\partial \lambda} - u^2 - \frac{\sigma^2}{2} \right), \quad (2.7)$$

$$135 \quad t = \frac{1}{\alpha g} (\lambda - u). \quad (2.8)$$

136 It should be noted that the variable σ is proportional to the total water depth.

$$137 \quad \sigma = 2\sqrt{gH} = 2\sqrt{g(-\alpha x + \eta)}, \quad (2.9)$$

138 so, the wave equation (2.4) is solved on the semi-axis $\sigma \geq 0$, and this coordinate plays the radius
 139 role in the cylindrical coordinate system. We would like to emphasize that the point $\sigma = 0$
 140 corresponds to a moving shoreline, and therefore, the original problem, solved in the area with a
 141 unknown boundary, is reduced to a fixed area problem.

142 It is important to note that the hodograph transformation is valid if the Jacobian
 143 transformation is non-zero

$$144 \quad J = \frac{\partial(x, t)}{\partial(\sigma, \lambda)} \neq 0. \quad (2.10)$$

145 It is the case when a gradient catastrophe, identified in the framework of the shallow-water
 146 theory with the wave breaking, does not occur. The necessary condition for the wave breaking
 147 absence is the boundedness and smoothness of all solutions; this question will be discussed
 148 further on.

149 We will assume that the wave approaches the coast from the area far from the shoreline (
 150 $x \rightarrow -\infty$), where the wave is linear. Then it is obvious that the function $\Phi(\sigma, \lambda)$ can be

151 completely found from the linear theory. The difficulty in finding the wave field in the near-
 152 shoreline area is due to the implicit transformation of the coordinates (x, t) to (σ, λ) . However,
 153 for the most interesting point of the moving shoreline $\sigma = 0$ (its dynamics determines the size of
 154 the flooded area on the coast) all the formulas become explicit. In particular, from (2.5) and (2.6)
 155 follows

$$156 \quad r(t) = R \left[t + \frac{u(t)}{\alpha g} \right] - \frac{u(t)^2}{2g}, \quad (2.11)$$

$$157 \quad u(t) = U \left[t + \frac{u(t)}{\alpha g} \right], \quad (2.12)$$

158 where $r(t)$ and $u(t)$ are the vertical displacement of the moving shoreline and its speed, and the
 159 functions $R(t)$ and $U(t)$ determine the field characteristics at the fixed point ($x = 0$) from the
 160 linear theory

$$161 \quad R(t) = \frac{1}{2g} \frac{\partial \Phi(\sigma = 0, \lambda)}{\partial \lambda} \Big|_{\lambda = \alpha g t}, \quad U(t) = \frac{1}{\sigma} \frac{\partial \Phi(\sigma, \lambda)}{\partial \sigma} \Big|_{\sigma = 0, \lambda = \alpha g t}. \quad (2.13)$$

162 Then we add the obvious kinematic relations for the vertical displacement and velocity of the last
 163 sea point along the slope.

$$164 \quad u(t) = \frac{1}{\alpha} \frac{dr(t)}{dt}, \quad U(t) = \frac{1}{\alpha} \frac{dR(t)}{dt}. \quad (2.14)$$

165 Let us note that formula (2.12) is identical to the so-called Riemann wave or a simple
 166 wave in a nonlinear non-dispersive medium (in particular, in nonlinear acoustics), if we consider
 167 the parameter $1/\alpha g$ to be a ‘coordinate’; see, for example, (Rudenko and Soluyan, 1977,
 168 Gurbatov et al, 1991, 2011). Moreover, formula (2.13) describes the integral over the Riemann
 169 wave. This analogy proves to be very useful when transferring the already known results in the
 170 wave nonlinear theory to the run-up characteristics described by the formulas (2.11) and (2.12)
 171 **ODE**.

172 Detailed calculations of the long wave run-up on the coast were carried out repeatedly;
 173 see, for example (Carrier and Greenspan, 1958; Synolakis, 1987; Pelinovsky and Mazova, 1992;
 174 Tinti and Toniti, 2005; Madsen and Fuhrman, 2008; Madsen and Schaffer, 2010; Antuano and
 175 Brocchini, 2008, 2010; Didenkulova, 2009; Dobrokhotov et al, 2015; Aydin and Kanoglu, 2017).

176 It is worth mentioning that the nonlinear time transformation in (2.11) and (2.12) leads to
 177 the shoreline oscillation distortion in comparison with the linear theory predictions. So, for large

178 amplitudes the wave shape becomes multi-valued (broken). The first moment of the wave
 179 breaking on the shoreline (the gradient catastrophe) is easily found from (2.12) by calculating the
 180 first derivative of the moving shoreline velocity

$$181 \quad \frac{du}{dt} = \frac{dU/dt}{1 - \frac{dU/dt}{\alpha g}}, \quad (2.15)$$

182 from it follows the wave breaking condition

$$183 \quad Br = \frac{\max(dU/dt)}{\alpha g} = \frac{\max(d^2R/dt^2)}{\alpha^2 g} = 1, \quad (2.16)$$

184 where we have introduced the breaking parameter Br to designate the left-hand side in (2.16),
 185 which characterizes the nonlinear wave properties on the shoreline. The condition (2.16) can be
 186 given a physical meaning, that the breaking occurs when the last sea particle acceleration ($\alpha^{-1}d^2R/dt^2$)
 187 exceeds the component of gravity acceleration along the shoreline ($g\alpha$). As
 188 shown in (Didenkulova, 2009), condition (2.16) coincides with (2.10) for Jacobian. It is
 189 important to emphasize that the breaking condition is unequivocally found through solving the
 190 linear problem of the wave run-up on the shore. It is determined only by the particle acceleration
 191 value on the shoreline; but it is not determined separately by the shoreline displacement or its
 192 velocity.

193 A similar Carrier – Greenspan transformation is obtained for waves in narrow inclined
 194 channels, fjords, and bays (Rybkin et al, 2013; Pedersen, 2016; Anderson et al, 2017; Raz et al,
 195 2018); only the wave equation (2.4) and relations (2.5) - (2.8) change. However, the moving
 196 shoreline dynamics is still described by equations (2.11) and (2.12), valid for arbitrary cross-
 197 section channels.

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199 **3. The moving shoreline dynamics at an initially monochromatic wave run-up**

200 The monochromatic wave run-up on a flat slope by using the Carrier – Greenspan
 201 transformation has been studied in a number of papers cited above. Let us reproduce here the
 202 main features of the moving shoreline dynamics necessary for us to draw the statistical
 203 description further on. Mathematically, the monochromatic wave run-up is described by an
 204 elementary solution of equation (2.4)

$$205 \quad \Phi(\sigma, \lambda) = QJ_0(l\sigma) \cos(l\lambda), \quad (3.1)$$

206 where Q and l are arbitrary constants, and J_0 is the zero-order Bessel function. Far from the
 207 shoreline ($\sigma \rightarrow \infty$) the Bessel function decreases, so the wave function Φ becomes small. In this
 208 case, in (2.5) - (2.8) one can use approximate expressions (the ‘linear’ Carrier – Greenspan
 209 transformation)

$$210 \quad \eta = \frac{1}{2g} \frac{\partial \Phi}{\partial \lambda}, \quad u = \frac{1}{\sigma} \frac{\partial \Phi}{\partial \sigma}, \quad x = -\frac{\sigma^2}{4\alpha g}, \quad t = \frac{\lambda}{\alpha g}, \quad (3.2)$$

211 and using the asymptotic representation for the Bessel function, reduce (3.1) to the expression
 212 for the water surface displacement

$$213 \quad \eta(x,t) = a(x) \left\{ \sin \left[\omega \left(t - \int \frac{dx}{\sqrt{gh(x)}} \right) \right] - \frac{\pi}{4} \right\} + \sin \left[\omega \left(t + \int \frac{dx}{\sqrt{gh(x)}} \right) + \frac{\pi}{4} \right], \quad (3.3)$$

214 where

$$215 \quad a(x) = \frac{Q}{2g} \sqrt{\frac{l}{\pi \sqrt{gh(x)}}}, \quad \omega = gl\alpha. \quad (3.4)$$

216 The wave field away from the shoreline is a superposition of two waves of the same frequency
 217 and a variable amplitude $a(x)$, which together form a standing wave. It immediately shows that
 218 the wave amplitude varies with depth according to the Green law ($h^{-1/4}$), as it should be far from
 219 the coast. The same asymptotic result follows from the exact solution of linear shallow water
 220 equations.

$$221 \quad \eta(x,t) = R_0 J_0 \left(\sqrt{\frac{4\omega^2 |x|}{g\alpha}} \right) \sin(\omega t), \quad (3.5)$$

222 where R_0 is the wave amplitude at the fixed shoreline ($x = 0$), identified with the maximum run-
 223 up height in the linear theory. By connecting (3.4) and (3.5), we obtain the formula for the run-
 224 up height obtained through the incident wave amplitude far from the coast

$$225 \quad \frac{R_0}{a(x)} = \sqrt{\frac{2\omega}{\alpha} \sqrt{\frac{h(x)}{g}}}. \quad (3.6)$$

226 Formula (3.6) allows working further with the run-up height R_0 instead of the wave amplitude far
 227 from the coast $a(x)$, ~~considering it to be given~~. **This run-up height will be considered as the given**
 228 **value**. Having determined Q and l through the incident wave parameters, we can calculate the
 229 run-up characteristics in the nonlinear theory, considering the limit of formula (3.1) with $\sigma \rightarrow 0$
 230 and using the Carrier – Greenspan transformation formulas (2.5) - (2.8). The moving shoreline
 231 movement is determined by the parametric dependence

232
$$t = \frac{\lambda}{\alpha g} - \frac{\omega R_0}{\alpha^2 g} \cos\left(\frac{\omega \lambda}{\alpha g}\right), \quad (3.7)$$

233
$$r = R_0 \sin\left(\frac{\omega \lambda}{\alpha g}\right) - \frac{\omega^2 R_0^2}{2\alpha^2 g} \cos^2\left(\frac{\omega \lambda}{\alpha g}\right). \quad (3.8)$$

234 It is convenient to introduce dimensionless variables

235
$$z = \frac{r}{R_0}, \quad \tau = \omega t, \quad \varphi = \frac{\omega \lambda}{\alpha g}, \quad (3.9)$$

236 and calculate the breaking parameter

237
$$Br = \frac{\omega^2 R_0}{\alpha^2 g}, \quad (3.10)$$

238 so the formulas (3.7) and (3.8) are finally rewritten in the form

239
$$\tau = \varphi - Br \cos(\varphi), \quad (3.11)$$

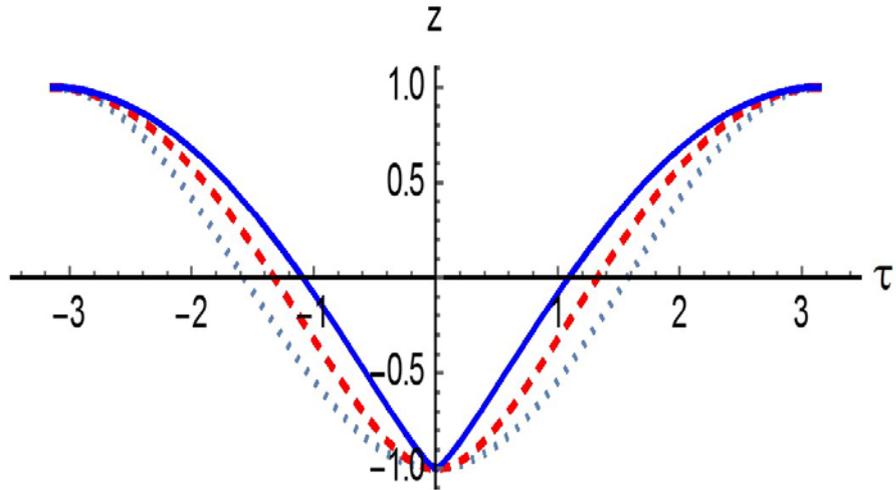
240
$$z = \sin(\varphi) - \frac{Br}{2} \cos^2(\varphi), \quad (3.12)$$

241 what is another ~~expression~~ ~~referred~~ for the formulas (2.11) and (2.12), if we take

242
$$R(t) = R_0 \sin(\omega t), \quad (3.13)$$

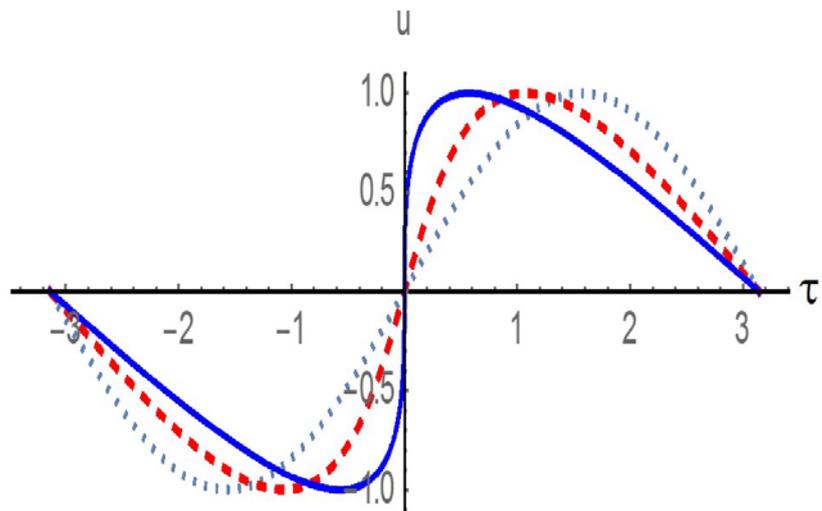
243 arising from (3.5) with $x = 0$. Let us note that the function $z(\tau, Br)$ is set in a parametric form,
 244 but after expressing φ from (3.12) and substituting it in (3.11), we can obtain the explicit
 245 expression for the function $\tau(z; Br)$. In the paper, we will use both explicit and implicit
 246 expressions of the functions describing the moving shoreline dynamics.

247 Fig. 2 shows the moving shoreline dynamics at different wave height values in terms of
 248 the breaking parameter up to the limiting value ($Br = 1$). In the limit of small parameter values,
 249 the oscillations are close to sinusoidal (it is almost a linear problem). Then, with the increasing
 250 amplitude, the moving shoreline velocity gets a steep leading front, while at the moving
 251 shoreline vertical displacement a peculiar feature is formed at the wave run-down stage. As it is
 252 known, at the time of the Riemann wave breaking, a peculiarity like $u \sim t^{1/3}$ is formed
 253 (Pelinovsky et al, 2013). Then, in the integral over the Riemann wave (at the moving shoreline
 254 displacement), this peculiar feature will have the form $z \sim t^{4/3}$. Thus, with the wave amplitude
 255 increase, the first breaking occurs at sea (at the run-down stage), and not on the coast. Then the
 256 breaking zone expands and moves on to the coast, but at this stage, analytical solutions based on
 257 the Carrier-Greenspan transformation become inapplicable.



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261

262 Fig. 2. The moving shoreline dynamics (top) and its velocity (below) in the case of the incident
 263 monochromatic wave for different breaking parameter values Br (0 – the dotted line, 0.5 – the
 264 dashed line and 1 – the solid line).

265

266 **4. Probabilistic characteristics of the initially sine wave run-up with a random phase**

267 Let us now consider the probabilistic characteristics of the initially sine wave run-up with a
 268 random phase on the shore, assuming it to be uniformly distributed over the interval $[0 - 2\pi]$.
 269 These characteristics are found by using the geometric probability methods (Kendall and Stuart,
 270 1969), so that for ergodic processes the probability density of the moving shoreline vertical

271 displacement coincides with the relative location time of the function $z(\tau)$ in the interval $(z,$
 272 $z + dz)$

$$273 \quad W(z) = \frac{1}{2\pi} \sum_{n=1}^N \left| \frac{d\tau_n}{dz} \right|, \quad (4.1)$$

274 where the summation takes place at all intersection levels $z(\tau)$. For harmonic disturbance, it is
 275 enough to restrict ourselves to considering the field on a half-period. So, for the moving
 276 shoreline vertical displacement in dimensionless variables, the derivative $d\tau/dz$ of the
 277 parametric curve (3.11) and (3.12) can be calculated through the ratio of the derivatives $d\tau/d\varphi$
 278 **and** $dz/d\varphi$

$$279 \quad W_z^{\sin}(z; Br) = \frac{1}{\pi} \frac{1 + Br \sin \varphi}{\cos \varphi + Br \cos \varphi \sin \varphi} = \frac{1}{\pi \cos \varphi}, \quad (4.2)$$

280 we indicated here that the probability density depends on Br as a parameter. Finding $\cos \varphi$ from
 281 the formula (3.12) for the vertical displacement, we obtain the final expression for the
 282 probability density

$$283 \quad W_z^{\sin}(z; Br) = \frac{1}{\pi} \frac{1}{\sqrt{1 - \frac{1}{Br^2} \left[1 - \sqrt{1 + 2zBr + Br^2} \right]^2}}, \quad (4.3)$$

284 which in the linear problem for a purely sinusoidal perturbation transforms into a well-known
 285 expression for the probability distribution of a harmonic signal with a random phase (Kendall
 286 and Stuart, 1969)

$$287 \quad W_z^{\sin}(z; 0) = \frac{1}{\pi} \frac{1}{\sqrt{1 - z^2}}. \quad (4.4)$$

288 The probability distribution (4.3) for the three values of the parameter Br is shown in
 289 Fig.3. As you can see, the probability density becomes an asymmetric function with a greater
 290 probability in the area of positive values corresponding to the wave run-up on the coast than at
 291 the run-down stage. At the ends of the interval, the probability density is unlimited throughout
 292 the entire range change of Br , since the shoreline oscillations near the maximum have a zero
 293 derivative (the moving shoreline velocity in it becomes zero).

294 The obtained probability density function can be used to calculate the statistical moments
 295 of the shoreline oscillations. Technically, however, it is easier to use the parametric equations
 296 (3.11) and (3.12) and calculate all the moments.

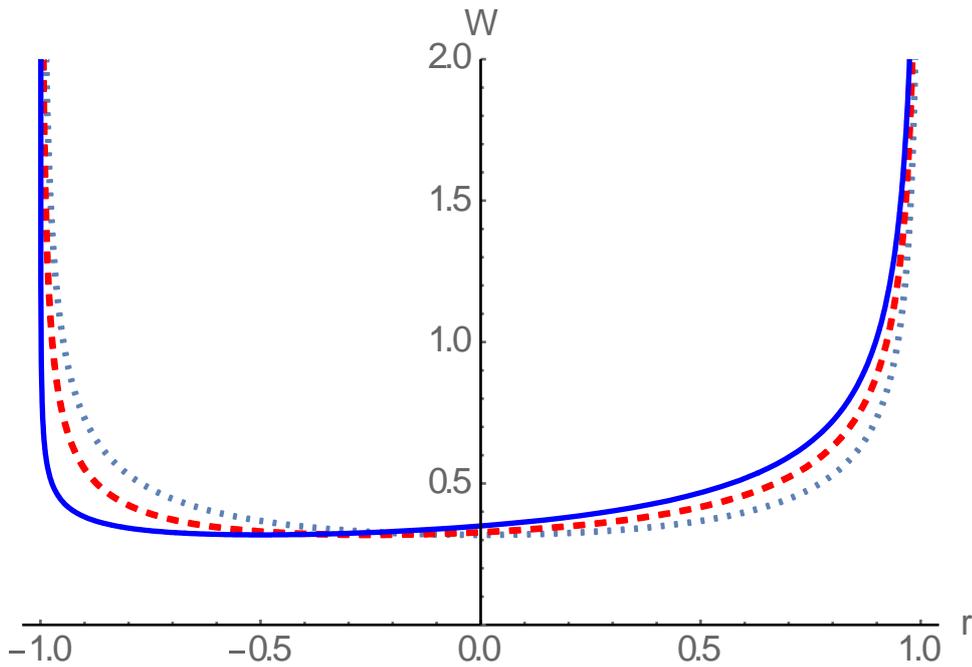
297
$$M_n^z = \frac{1}{2\pi} \int_0^{2\pi} z^n(\tau) d\tau = \frac{1}{2\pi} \int_0^{2\pi} z^n(\varphi) \frac{d\tau}{d\varphi} d\varphi . \quad (4.5)$$

298 So, the first moment

299
$$M_1^z = \frac{Br}{4} \quad (4.6)$$

300 determines the average water level rise on the coast when the waves approach the shore (set-up
301 phenomenon), which is commonly observed (Dean and Walton, 2009).

302



303
304 Fig. 3. The probability density of the moving shoreline vertical displacement for the initially sine
305 wave run-up at $Br = 0$ (the dotted line), 0.5 (the dashed line) and 1 (the solid line).

306

307 The second moment determines the dispersion

308
$$\delta^2 = \frac{1}{2\pi} \int_0^{2\pi} (z - M_1^z)^2 d\tau = \frac{1}{2} - \frac{3}{32} Br^2 , \quad (4.7)$$

309 characterizing the fluctuation range relative to the average value; it relatively weakly decreases
310 with the growth of the parameter Br (less than 10% for non-breaking waves).

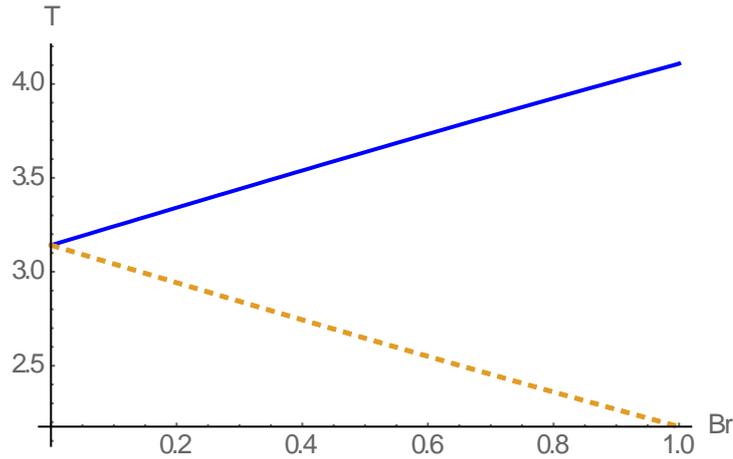
311 Finally, the total flooding time and its drainage time are easy to find from (3.11) and
312 (3.12), finding from the equation (3.12) mentioned last, the value φ , at which $z = 0$, and
313 substituting the obtained values in (3.11)

314
$$T_{flood} = \pi - 2 \arcsin \left[\frac{\sqrt{1 + Br^2} - 1}{Br} \right] + 2\sqrt{2} \sqrt{\sqrt{1 + Br^2} - 1},$$

315 (4.9)

316
$$T_{dry} = \pi + 2 \arcsin \left[\frac{\sqrt{1 + Br^2} - 1}{Br} \right] - 2\sqrt{2} \sqrt{\sqrt{1 + Br^2} - 1},$$

317 Both times change almost linearly with the increasing wave amplitude (parameter Br), see Fig. 4.



318 Fig. 4. The total flooding time (the solid curve) and the drainage time (the dashed curve)

319 depending on the parameter Br .

320

321

322 It is worth noting that, in contrast to the vertical displacement, the moving shoreline

323 velocity distribution $[u = (\omega R_0 / \alpha)v]$, as it is easy to show, does not depend on the breaking

324 parameter and probability density function is determined by the simple formula

325
$$W_v^{\sin}(v) = \frac{1}{\pi} \frac{1}{\sqrt{1-v^2}}. \quad (4.10)$$

326 The distribution independence on the degree of nonlinearity is well known for the Riemann

327 waves and is explained by the compensation of compression and rarefaction areas (Gurbatov et

328 al, 1991, 2011).

329

330 **5. Probabilistic characteristics of a narrow-band wave run-up with a random amplitude**

331 **and phase**

332 Let us consider the run-up of a quasi-harmonic wave with a random amplitude and phase

333 on a flat slope. To do this, we will first rewrite formulas (4.3) and (4.10) for them to include the

334 wave amplitude. It is convenient to enter the maximum height R_{max} as the amplitude scales at
 335 which the breaking parameter turns into 1

$$336 \quad Br = \frac{\omega^2 R_{max}}{\alpha^2 g} = 1, \quad (5.1)$$

337 and to use dimensionless displacement ($y=r/R_{max}$). Then the dimensionless amplitude is

$$338 \quad A = \frac{R_0}{R_{max}} \leq 1, \quad (5.2)$$

339 and formula (4.3) is converted to the form ($-A < y < A$)

$$340 \quad W_y^{\sin}(y; A) = \frac{1}{\pi} \frac{1}{\sqrt{A^2 - \left[1 - \sqrt{1 + 2y + A^2}\right]^2}}. \quad (5.3)$$

341 Assuming now that the wave amplitude A is a random variable, we average (5.3) by using
 342 the amplitude distribution density $W_A(A)$

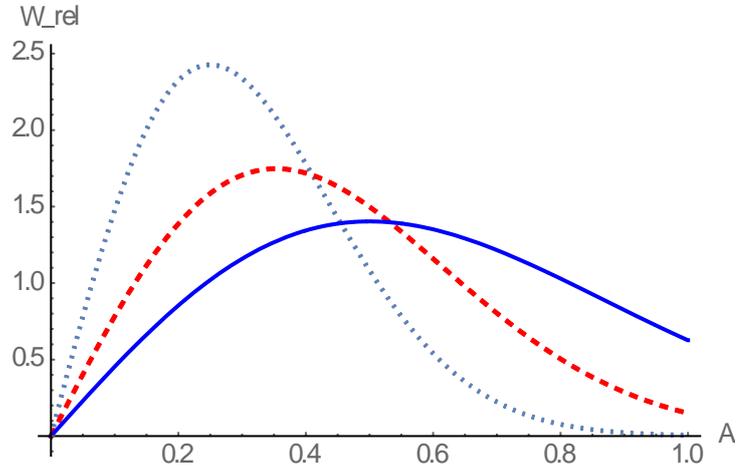
$$343 \quad W(y) = \int_y^{\infty} W_y^{\sin}(y; A) W_A(A) dA. \quad (5.4)$$

344 Formula (5.4) has an important practical meaning: by the measured distribution of the wave
 345 amplitudes far from the coast (re-computed on run-up amplitudes in the linear theory), it is
 346 possible to obtain the distribution of the wave run-up characteristics on the coast. The only
 347 requirement imposed on the wave ensemble is that it should not contain breaking waves, which
 348 should be somehow removed from the record. It immediately follows that the Gaussian field
 349 containing large amplitude tails does not fit this requirement, and it should be modified.
 350 Therefore, we assume the amplitude distribution to be finite for $A < A_{max} = 1$. **The narrow-band**
 351 **random wave field contains sine waves with almost constant frequency and random amplitude**
 352 **and phase. It means that if the wave amplitude is below the “breaking amplitude” $A_{max} = 1$, the**
 353 **breaking will not be implemented in any way, and the random wave run-up will take place**
 354 **without any breaking. Further calculations depend on the specific type of the amplitude**
 355 **distribution.**

356 Let us construct the finite amplitude distribution at which the linear field distribution is
 357 close to the Gaussian form and modify the Rayleigh distribution **for wave heights** in the area
 358 $A < A_{max} = 1$ (Fig. 5)

$$359 \quad W_A(A; A_{max}, A_s) = \frac{1}{1 - \exp(-2A_{max}^2 / A_s^2)} \frac{4A}{A_s^2} \exp\left(-2\frac{A^2}{A_s^2}\right), A \leq A_{max}, \quad (5.5)$$

360 to make the density function distribution normalized. Here, A_s is the so-called significant wave
 361 run-up height (an averaged value of 1/3 highest amplitudes). We would like to note here, that it
 362 follows from (2.11) and (2.12) that the extremal run-up characteristics in the nonlinear theory
 363 remain the same as in the linear theory. This means that the significant wave run-up height
 364 remains the same as in the nonlinear theory.



365

366

367 Fig. 5. The modified Rayleigh distribution (5.5) for different distribution values A_s/A_{max} ;
 368 0.5 – the dotted curve, 0.7 – the dashed line, 1 – the solid line.

369

370 When $A_s \ll A_{max} = I$, distribution (5.5) transforms into the Rayleigh one, which is
 371 characteristic of the Gaussian initial distribution of a narrow-band random signal. With the help
 372 of (5.5), it becomes possible to calculate the distribution function of shoreline oscillations for the
 373 various wave energy. So, with the incident wave small amplitude ($A_s \ll I$), distribution (5.3) can
 374 be replaced by a simpler expression (4.4) and the answer is the run-up distribution characteristics
 375 in the linear theory:

$$376 \quad W_{lin}(y; A_{max}, A_s) = \frac{4}{\pi A_s^2 [1 - \exp(-2A_{max}^2 / A_s^2)]} \int_y^{A_{max}} \frac{A}{\sqrt{A^2 - y^2}} \exp\left(-2 \frac{A^2}{A_s^2}\right) dA. \quad (5.6)$$

377 Besides, if $A_s \ll A_{max} = I$, the integral (5.6) is reduced to the Gaussian distribution

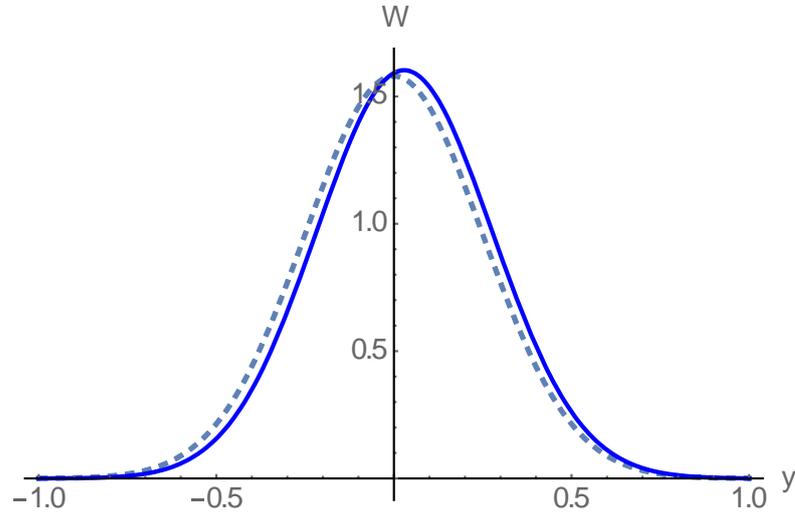
$$378 \quad W_{lin}(y; A_s) = \frac{2}{\sqrt{2\pi} A_s} \exp\left(-2 \frac{y^2}{A_s^2}\right), \quad (5.7)$$

379 where, $A_s = 2\sigma_y$, and σ_y^2 is the moving shoreline oscillation dispersion.

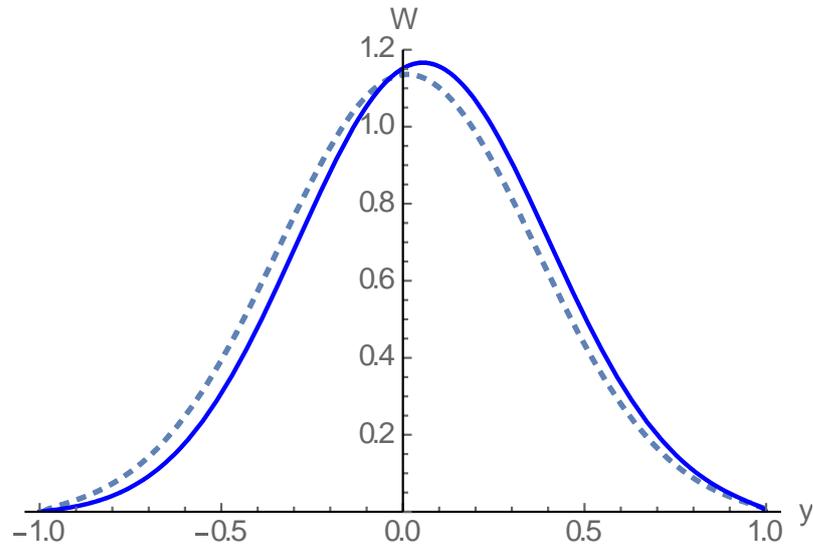
380 Fig. 6 shows the distribution of the run-up characteristics for different ratios of A_s/A_{max}
 381 values by formulas (5.4) and (5.5); they are shown in solid lines. Here the dashed lines show the

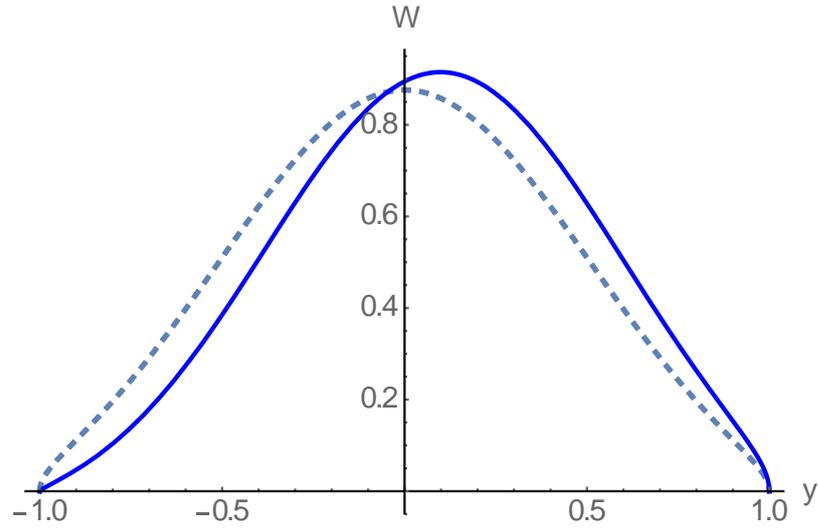
382 calculation results according to the linear theory (5.6). As one can see, with $A_s/A_{max} = 0.5$ (the top
383 panel) and 0.7 (the middle panel), the linear distribution is close to the Gaussian one.
384 Nonlinearity leads to the asymmetry of the distribution function density in the direction of
385 positive values corresponding to the wave characteristics on the coast. If the undisturbed wave
386 ensemble is made of relatively large waves ($A_s/A_{max} = 1$), their distribution is far from the
387 Gaussian, both in the linear and in the nonlinear approximation.

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Fig. 6. The probabilistic density function of the vertical shoreline displacement in the nonlinear theory (solid lines) and in the linear theory (dashed lines) for different A_s/A_{max} : 0.5 values: (the upper panel), 0.7 (the middle panel) and 1 (the lower panel).

The finite ($A < A_{max}$) power-law distribution concentrated mainly near the maximum amplitude A_{max} can be considered as another example of undisturbed large-amplitude waves.

397

$$W_A(A) = \frac{6A^5}{A_{max}^6}. \quad (5.8)$$

398

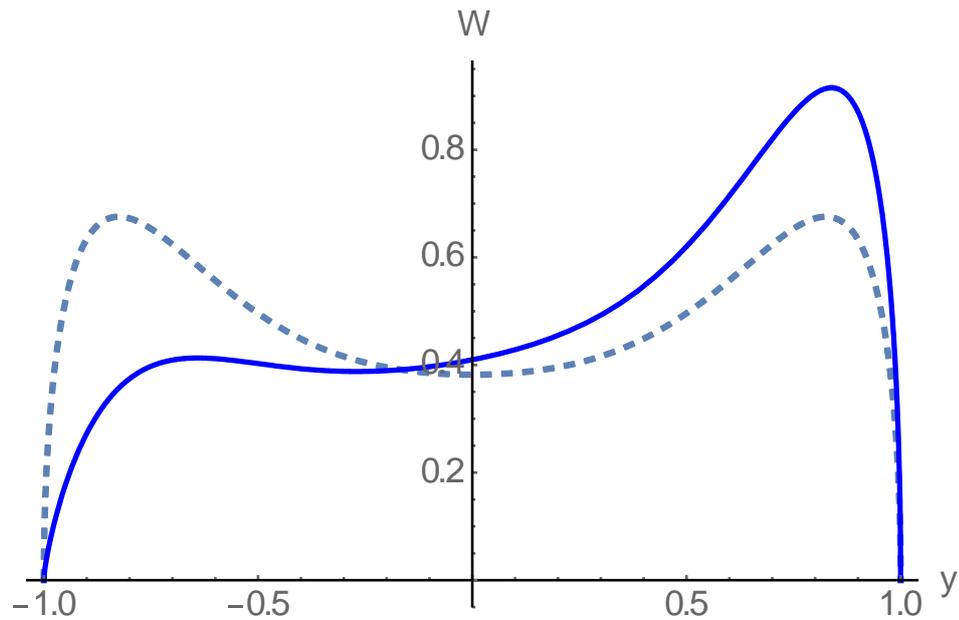
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Fig. 7 shows the graphs of the probabilistic density function of the moving shoreline displacement calculated by using formulas (5.4) and (4.4) in the linear theory and (5.3) in the nonlinear theory. It is also seen in the figure that nonlinear effects lead to a strong asymmetry towards the positive values, that is, to the wave amplification at the run-up up stage than at the run-down stage.



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Fig. 7. Probabilistic density function of the shoreline vertical displacement in the linear theory (the dashed line) and non-linear theory (the solid line)

6. The wave breaking effect on probabilistic run-up characteristics

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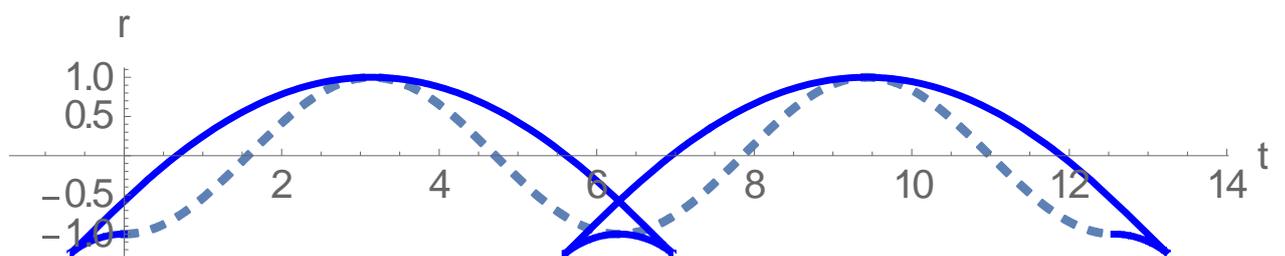
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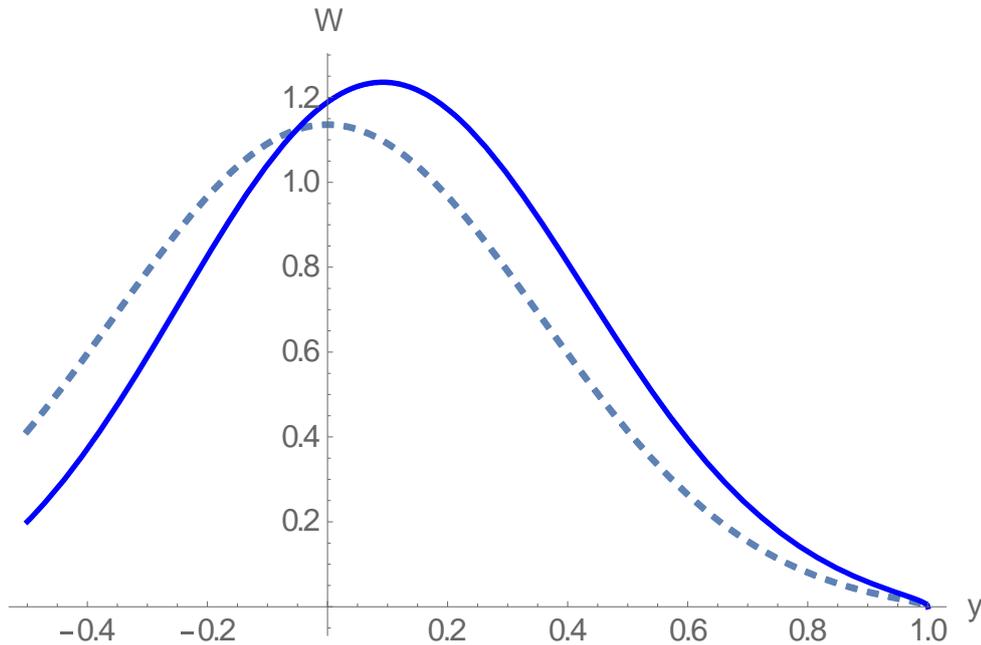
The theory described above is valid for non-breaking waves. The mentioned wave ensemble, strictly speaking, cannot be the Gaussian one, as it always has unlimited tails in the probability density function. Let us briefly discuss what the formulas obtained for non-breaking waves lead to in the presence of broken waves. Fig. 8 shows the parametric curve (3.11) - (3.12) when $Br = 2$. Formally, the curve became multi-valued in the range of negative values corresponding to the maximum water outflow from the coast. We have already indicated that the probability density function of the moving shoreline vertical displacement $W(\xi)$ coincides with the relative residence time $\xi(t)$ of the function in the interval $(\xi, \xi + d\xi)$, which is calculated by formula (3.1). In contrast to negative cut-off bias values, in the area of positive values there is no ambiguity, and, therefore, all the calculations can be carried out by using the formulas described above. An example of such calculation with $Br = 2$ and $r > -0.5$ (in the zone of one-value solution) is shown in Fig. 9.

420



421

422 Fig. 8. The parametric curve (3.11) - (3.12) with $Br = 2$ (the solid curve) in comparison with the
423 linear problem with $Br = 0$ (the dashed line)



424

425 Fig. 9. The probability density function at $Br = 2$, constructed by formulas (5.3), (5.4) and (5.5)
426 (the solid line) in comparison with the linear distribution (5.6) is the dotted line. $A_s/A_{max} = 0.7$.

427

428 However, these results should be treated with caution. **If $Br > 1$ the Jacobian breaks down**
429 **seawards of the shoreline. This may affect the probabilistic distribution on the positive side.** This
430 important issue requires going beyond the theory discussed in this article.

431

432

433

434 7. Discussion and conclusion

435

436 In this paper, we study the run-up of irregular narrow-band waves with a random
437 envelope (swell, storm surges, and tsunami) on a beach of a constant slope. The work was
438 carried out in the framework of the nonlinear wave theory with one important assumption: there
439 should be no breaking waves in the wave ensemble. This restriction is quite strict for field and
440 laboratory conditions, but nevertheless, there are cases when it is performed. For instance, 75%
441 of historical tsunami waves climbed on the coast with no breaking (Mazova et al, 1983). In the
442 experiments performed in the Warwick University tank and in the Large Tank in Hannover
(Denissenko et al, 2011, 2013), this condition was fulfilled.

443 The wave nonlinearity at the run-up stage leads to increased deviations from Gaussianity, as
444 might be expected from general considerations. Nevertheless, it is shown that the probability
445 distribution of the moving shoreline velocity does not depend on the wave nonlinearity and can
446 be calculated within the linear theory framework. The same conclusion can be drawn about the
447 distribution of the extreme run-up characteristics (the moving shoreline displacement and speed),
448 which, in fact, has already been discussed earlier (Didenkulova et al, 2008). However, the
449 probabilistic density function of the moving shoreline displacement differs from that predicted
450 one in the linear theory framework. It is described by formula (5.4) by using either the
451 theoretical or the measured distribution of the incident wave amplitudes. The paper gives the
452 calculation results of the probable run-up characteristics with a modified Rayleigh distribution
453 for wave amplitudes.

454 The wave breaking leads to the inapplicability of the wave run-up theory based on the
455 Carrier-Greenspan transformation. If, nevertheless, the share of large amplitude waves is small,
456 the breaking occurs mainly at the run-down stage, having little effect on the long-wave coast
457 flooding characteristics (see Section 6). This question, however, requires a special study based
458 on direct numerical solutions of the shallow-water equations or their nonlinear-dispersive
459 generalizations.

460 Finally, it is worth noting that we considered the narrow-band wave run-up with a
461 random amplitude and phase; as for the random waves with a wide spectrum – it is the problem
462 of further consideration.

463 The obtained probability density functions of the vertical displacement of the moving
464 shoreline are useful to compute statistical characteristics of flooding time and force on coasts and
465 constructions, which are necessity for the mitigation of natural marine hazards.

466 *Now in practice various generalizations of shallow-water equations are used to analyze
467 tsunami runup including wave dispersion, see for instance (Lovholt et al, 2012). Wave dispersion
468 as a quadratic dissipative term that prevents us from getting analytical results, so their influence
469 on statistical characteristics should be investigated in future.*

470 **Acknowledgment:**

471 The work is supported by the grants from the Russian Science Foundation: No.19-12-00256 (in
472 part of computing the random Riemann wave characteristics) and No. 19-12-00253 (in part of
473 computations the probability density function of the moving shoreline).

474

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